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Residual stress in AlN films grown on sapphire substrates by molecular beam epitaxy



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ABSTRACT

Residual stress in AlN films grown by molecular beam epitaxy (MBE) has been studied by Raman scattering spectroscopy. A strain-free Raman frequency and a biaxial stress coefficient for $E_2(\text{high})$ mode are experimentally determined to be $657.8 \pm 0.3 \text{ cm}^{-1}$ and $2.4 \pm 0.2 \text{ cm}^{-1}/\text{GPa}$, respectively. By using these parameters, the residual stress of a series of AlN layers grown under different buffer layer conditions has been investigated. The residual compressive stress is found to be obviously decreased by increasing the Al/N beam flux ratio of the buffer layer, indicating the generation of tensile stress due to stronger coalescence of AlN grains, as also confirmed by the *in-situ* reflection high energy electron diffraction (RHEED) monitoring observation. The stronger coalescence does lead to improved quality of AlN films as expected.

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1. Introduction

Recently, AlGaIn-based quantum devices have attracted much research attention in the areas of electrical engineering, material science, and physics due to the numerous potential applications such as ultraviolet solid-state light sources, solar-blind photodetectors and so on [1,2]. Among the III-nitride semiconductors, AlN is always regarded as a preferred device substrate or template material for crack-free fabrication. Up to now, great progress has been made for the growth of either bulk AlN or AlN templates [3–6]. However, the device performance is still greatly limited by the strain-induced bending or cracks in thick AlN films commonly grown by hetero-epitaxy on sapphire, Si or SiC substrates [7,8]. In this sense, residual stress analysis in layered structures is of great importance for understanding the mechanical properties of AlN films and helps to adjust the strain status for crystalline quality improvement. Among all the techniques, Raman scattering spectroscopy provides a contactless, non-destructive and sensitive tool to characterize the stress distribution, making it an essential and potential way for residual stress analysis [9]. Generally, the biaxial stress distribution can be easily acquired by the linear

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dependence of biaxial stress on $E_2(\text{high})$ phonon frequency using the obtained strain-free Raman frequency and biaxial stress coefficient. Some efforts have been performed on this issue and both theoretical and experimental results have been explored [10–13]. However, most reports focused on MOCVD-grown or HVPE-grown templates which somehow disagreed with the theoretical values and the contradictions were not well explained. Few reports are available to precisely determine the above parameters from AlN films grown by molecular beam epitaxy (MBE).

MBE supplies us a way to obtain atomically flat and high-purity AlN templates. The avoidance of oxygen contamination is of great importance towards the high-quality AlGaN quantum wells [14,15]. In the early work, we have obtained a much broad growth window for droplet-free AlN films with step-flow feature [16]. But the crystalline quality can still be further improved through studying the strain states in the epi-layers. In this work, the crystalline quality of MBE-grown AlN films was improved by increasing the Al/N beam flux ratio during AlN buffer layer growth. Residual stress analysis showed that this improvement originated from a stronger AlN grains coalescence for higher Al/N ratio. This analysis is based on the obtained values of the biaxial stress coefficient and strain-free Raman frequency for $E_2(\text{high})$ mode, which have been experimentally determined in this work and found to be well in accord with the theoretically predicted values.

2. Experimental

The growth of AlN films was performed on the 2-inch c-plane sapphire substrates by plasma-assisted MBE system (SVTA). Reflection high energy electron diffraction (RHEED) and an optical reflection spectrometer are used to *in-situ* monitor the whole growth process. Sapphire substrate was first thermally cleaned at 1000 °C for an hour. Then, nitridation was performed at 800 °C for half an hour, leading to the formation of very thin AlN layer on the surface. AlN layers were then deposited by using low temperature AlN buffer layer. To evaluate the residual strain, tens of samples were selected at different growth conditions such as varied growth temperature, Al/N ratio and thickness as ever reported [16]. To study the effect of buffer layer growth condition on quality improvement, five samples with common structure of 30-nm-thick AlN buffer layers and 360-nm-thick AlN top layers were grown. Another sample without buffer layer, as a reference, was also grown. All the growth process is kept the same except that the Al/N ratio changes monotonically during the buffer layer growth. The lattice constants of the AlN films have been determined by high-resolution X-ray diffraction (XRD) measurements using $K\alpha_1$ ($\lambda = 0.15$ nm) radiation. Residual stress was estimated by Raman spectroscopy at room temperature in $z(x, x)$ - z backscattering geometry using a laser excitation source at a wavelength of 514 nm.

3. Results and discussion

To study the biaxial residual stress in hexagonal AlN by Raman scattering measurement, one usually pays attention to $E_2(\text{high})$ mode since it corresponds to atomic oscillations in the c-plane [17]. Two parameters are important to study stress, i.e. strain-free Raman frequency for $E_2(\text{high})$ mode and the Raman biaxial stress coefficient (k). The in-plane residual stress (σ_a) can be derived by using $\sigma_a = k^{-1} \Delta\omega[E_2(\text{high})]$, where $\Delta\omega[E_2(\text{high})]$ is the strain-induced Raman frequency shift for $E_2(\text{high})$ mode. To determine the biaxial stress coefficient as accurate as possible, Raman scattering measurements were performed on a large number of samples grown on sapphire substrates by MBE. Fig. 1(a) shows a typical Raman scattering spectrum for AlN layer grown on the sapphire substrate, where several scattering peaks are observed. The peaks located at 657 and 890 cm^{-1}

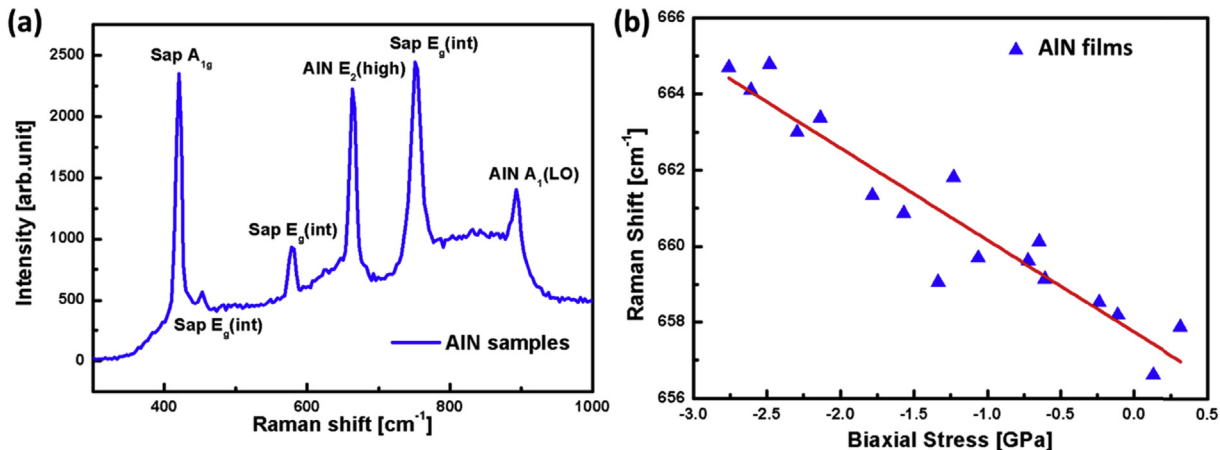


Fig. 1. (a) A typical Raman spectrum of MBE-grown AlN films on sapphire. Visible are the $E_2(\text{high})$ and $A_1(\text{LO})$ modes in AlN films as well as A_{1g} and $E_g(\text{int})$ modes in sapphire substrate. (b) Raman frequencies of $E_2(\text{high})$ phonon mode as a function of residual biaxial stress. The red line shows a linear fit to the data, which gives a strain-free phonon frequency of 657.8 ± 0.3 cm^{-1} and a biaxial stress coefficient of 2.4 ± 0.2 $\text{cm}^{-1}/\text{GPa}$ for the $E_2(\text{high})$ mode. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

are assigned to the $E_2(\text{high})$ and $A_1(\text{LO})$ modes, respectively [17]. Other peaks located at 578 and 751 cm^{-1} are two scattering peaks from $E_g(\text{int})$ phonon modes, while the one located at 418 cm^{-1} is A_{1g} mode of sapphire substrate [18,19]. The typical line widths of scattering peaks from the $E_2(\text{high})$ mode of the AlN films are 5–8 cm^{-1} , which indicates good crystalline quality considering that the thickness of AlN layers is less than 400 nm.

Then, residual stress in AlN layer can be estimated by using XRD measurement, where the stress is derived from the deformation of lattice constant. The out-of-plane strain (ϵ_c) can be obtained by using $\epsilon_c = (c - c_0)/c_0$, where c is measured lattice constant and $c_0 = 0.49792$ nm is the lattice constant of free-standing AlN [11]. Assuming Hooke's law for elastic deformation, there is $\epsilon_c/\epsilon_a = -2\nu/(1 - \nu)$, and the biaxial stress σ_a can be obtained by:

$$\sigma_a = \left(C_{11} + C_{12} - \frac{2C_{13}^2}{C_{33}} \right) \epsilon_a \quad (1)$$

where ν is the Poisson ratio with a value of 0.19 [11], C_{ij} is the stiffness constants with values of $C_{11} = 345$ GPa, $C_{12} = 125$ GPa, $C_{13} = 120$ GPa, $C_{33} = 395$ GPa [12].

Fig. 1 (b) shows the variation of Raman frequencies of $E_2(\text{high})$ mode as a function of residual stress σ_a determined by MBE-grown samples. Here negative values of biaxial stress indicates compressive stress while positive value represents tensile one. The Raman frequency of $E_2(\text{high})$ mode is linearly changed with biaxial stress as shown as the red fitting line. A biaxial stress coefficient k of $2.4 \pm 0.2 \text{ cm}^{-1}/\text{GPa}$ is obtained by the best fit and strain-free Raman frequency for $E_2(\text{high})$ mode is determined to be $657.8 \pm 0.3 \text{ cm}^{-1}$. The latter value coincides well with the reported value of 657.4 cm^{-1} as determined from free-standing AlN [20,21]. The $k = 2.4 \pm 0.2 \text{ cm}^{-1}/\text{GPa}$ is lower than previously reported 4.04 ± 0.3 and $2.9 \pm 0.3 \text{ cm}^{-1}/\text{GPa}$, but is very close to the theoretically predicted value of $2.5 \text{ cm}^{-1}/\text{GPa}$ [10,13,22]. With these values, residual stress of MBE-grown AlN films can be easily analyzed by Raman scattering measurement.

Let us turn to the influence of AlN buffer layer on quality improvement and their stress correlation. To improve the crystalline quality, we have used AlN buffer layers which are grown at 800 °C with a thickness of 30 nm before the growth of 360-nm-thick high temperature top layers at 950 °C. The growth rate was set at 6 nm/min, and the Al/N beam flux ratio of AlN top layer was kept as 2.9. The conditions for all AlN samples are the same except that the Al/N beam flux ratios in buffer layers are 0, 1.0, 1.2, 1.4, 1.9, and 2.4, respectively. Here the sample with an Al/N ratio of 0 means one without AlN buffer layer. As shown in Fig. 2, the two red lines represent the FWHMs of XRD ω -scans for symmetric (002) and asymmetric (102) planes of the above samples. Obviously the FWHMs values of XRD ω -scans for symmetric (002) plane are almost independent of the Al/N beam flux ratio. However, the FWHMs values of XRD ω -scans for asymmetric (102) plane become smaller with increasing the Al/N beam flux ratio. As we know, the FWHMs value of (002) XRD ω -scans refers to the density of threading dislocations with screw component while that of (102) XRD ω -scans refers to ones with edge component. Therefore, the density of edge-type threading dislocations is reduced with increasing the Al/N beam flux ratio for the AlN buffer layer growth.

To figure out why the crystalline quality could be improved with increasing Al/N beam flux ratio during the growth of buffer layer, the residual stress analysis by Raman scattering was performed. The residual stress, which was evaluated by using the obtained strain-free Raman frequency and biaxial stress coefficient above, is displayed by the blue line in Fig. 2. It is shown that all samples exhibit compressive stress and this compressive stress is reduced with increasing the Al/N beam flux ratio in the buffer layer growth. As we know, there are basically three origins for the residual biaxial stress in the AlN layer. First, the lattice mismatch between AlN and sapphire is 13%, which would lead to residual compressive stress [23]. However, it can't be the main source since the AlN layer would be quickly relaxed during the initial 6–7 monolayers growth. Second, the

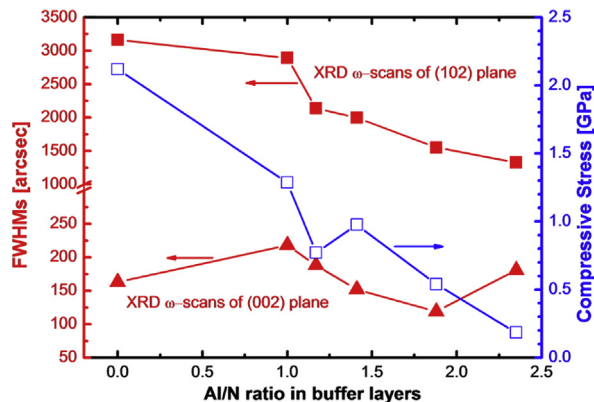


Fig. 2. Crystalline quality by XRD measurements and compressive stress status of AlN/sapphire structures at different Al/N beam flux ratio in buffer layers. The red line with solid triangles represents (002)-plane FWHMs values of XRD ω -scans, meanwhile the red line with solid squares stands for (102)-plane FWHMs values of XRD ω -scans. The blue line with open squares illustrates the compressive stress intensity. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

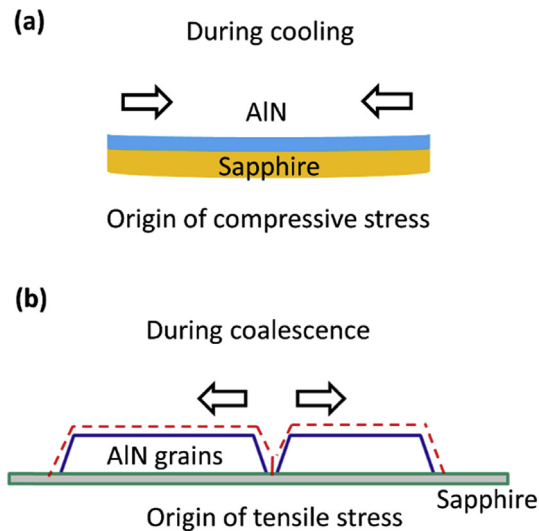


Fig. 3. The schematic diagram of the origins of compressive stress during cooling process (a) and tensile stress during coalescence one (b).

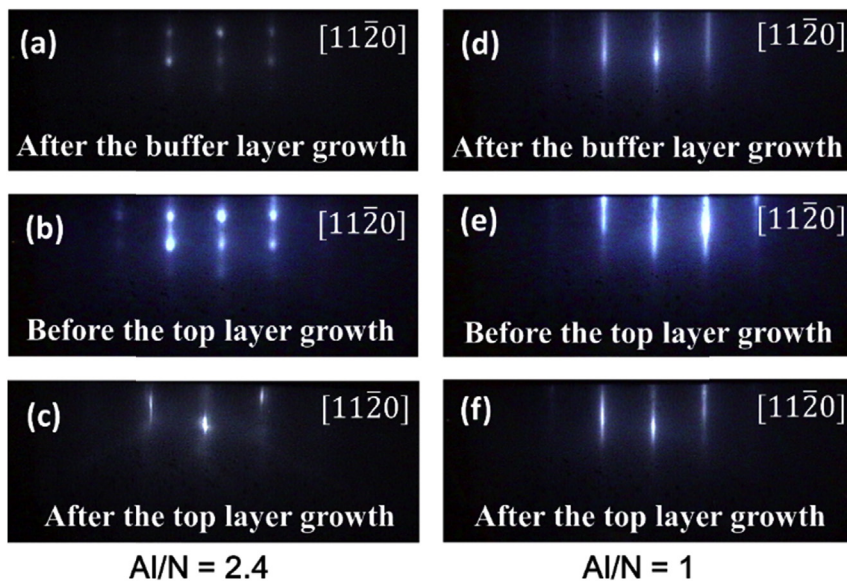


Fig. 4. RHEED patterns along $[11\bar{2}0]$ azimuth recorded at that moment after the buffer layer growth (a)/(d), before the top layer growth (b)/(e) and after the top layer growth (c)/(f) with Al/N beam flux ratios of 2.4/1, respectively.

thermal expansion coefficient of AlN is much smaller than that of sapphire [17]. Consequently, the shrink of sapphire lattice is more intense than AlN lattice and compressive stress would be generated during cooling down of samples, as displayed in Fig. 3 (a). Third, a large number of tensile stress will be generated by the coalescence process of crystal grains during the growth or the annealing process, as demonstrated in Fig. 3 (b). Therefore, the residual stress in AlN layer mainly depends on the competition between the cooling and coalescence process. In our experiment, the compressive stress generated during sample cooling down plays a dominant role since all the samples exhibit the residual compressive strain, and the compressive stress is effectively compensated by increasing the Al/N ratio in buffer layer growth. Considering all the growth conditions are the same except the Al/N ratios, the reduction of residual compressive stress could be attributed to the increase of tensile stress generated by the improved AlN grains coalescence for higher Al/N ratio. This strong coalescence leads to the improvement of crystalline quality.

The evidence is shown in Fig. 4, which records the RHEED patterns after buffer growth, before and after top layer growth, respectively. Fig. 4 (a, b, c) present RHEED patterns of the sample buffered with Al/N beam flux ratio of 2.4, and Fig. 4 (d, e, f) present ones buffered with Al/N ratio of 1. A streaky pattern is a typical feature for 2D growth mode while spotty one is for 3D

mode. It can be seen that both samples experience the 3D growth mode at first and then are followed by the 2D growth mode. For the sample buffered with higher Al/N beam flux ratio, bigger islands were formed due to the stronger coalescence after the growth of buffer layer, leading to the maintenance of the 3D growth mode during the whole buffer layer growth process. However, as to the sample buffered with lower Al/N beam flux ratio, the coalescence of AlN grains was much weaker and the growth of buffer started in 3D mode and quickly change into 2D growth mode after 10 nm deposition of AlN buffer layer. As we know, the edge-type threading dislocations will stretch among the boundary of the islands, and the dislocation density is in reverse proportion to the size of the islands [24]. Consequently, the density of edge-type threading dislocations is decreased due to the stronger coalescence with increasing Al/N beam flux ratio during the growth of AlN buffer layer.

4. Conclusions

We have experimentally determined the strain-free Raman frequency for $E_2(\text{high})$ mode and biaxial stress coefficient with values of $657.8 \pm 0.3 \text{ cm}^{-1}$ and $2.4 \pm 0.2 \text{ cm}^{-1}/\text{GPa}$, which are in good agreement with the theoretical prediction. The Raman scattering on AlN films under different Al/N beam flux ratios during the growth of AlN buffer showed that the residual compressive stress decreased with increasing Al/N beam flux ratio. *In-situ* monitoring demonstrated a stronger coalescence in AlN buffer layer during the growth for a higher Al/N ratio, resulting in the improved crystalline quality of AlN epi-layers.

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